# A Redetermination of the Distribution of Atoms in Cu<sub>5</sub>Zn<sub>8</sub>, Cu<sub>5</sub>Cd<sub>8</sub>, and Cu<sub>9</sub>Al<sub>4</sub>

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The atomic distribution in gamma brass, Cu<sub>2</sub>Zn<sub>8</sub>, has been established by neutron powder diffraction. It is of the Au<sub>5</sub>Zn<sub>8</sub> type. The structures of Cu<sub>5</sub>Cd<sub>8</sub> and Cu<sub>5</sub>Al<sub>4</sub> have been refined from single-crystal diffractometer data and the distribution of atoms in these structures reconfirmed.

Cu<sub>5</sub>Zn<sub>8</sub> is the prototype of the gamma-brass structure (D8<sub>1-3</sub>), and was characterized as such by Westgren and Phragmén 1 at this Institute in 1925. The structure was investigated by Bradley and Thewlis, 2 and refined by Bradley and Gregory 3 who determined the position parameters of the atoms, but could only infer the ordering scheme (D8<sub>2</sub>) by analogy with the ordering in Au<sub>5</sub>Zn<sub>8</sub> since, with X-rays, it was not possible to tell the difference between Cu and Zn. Furthermore, the atomic distribution assumed in Cu<sub>5</sub>Zn<sub>8</sub> differs from that in Cu<sub>5</sub>Cd<sub>8</sub>.3 Thus, it was concluded that a redetermination of the atomic distribution in both these phases was well warranted.

A refinement of the Cu<sub>9</sub>Al<sub>4</sub> structure 4 based upon single crystal diffracto-

A refinement of the Cu<sub>9</sub>Al<sub>4</sub> structure <sup>4</sup> based upon single crystal diffractometer data was carried out and published by one of the present authors.<sup>5</sup> Some peculiarities remained, however, at the end of the refinement, especially in the temperature factors of the aluminum atoms. Since the least-squares calculations were carried out with a program which could only handle orthorhombic and lower symmetries, it was deemed to be of value to repeat the refinement, using the old data, with a program suited to the treatment of cubic symmetry.

#### **EXPERIMENTAL**

The starting materials copper (elektrolytkoppar, granular,  $\geq 99.9$  % Cu, Kebo AB), zinc (granular, Mallinckrodt Analytical Reagent) and cadmium (sticks, specially pure, the British Drug Houses, 99.9 % Cd) were weighed out to match the compositions  $\mathrm{Cu_5Zn_8}$  and  $\mathrm{Cu_5Cd_8}$ . The components were heated together at  $\sim 1000^\circ\mathrm{C}$  in sealed, evacuated silica capsules until reaction was complete. This was checked by quenching of the capsules

in water, extraction and crushing, in a steel mortar, of the solidified alloy pellets to make sure that they were homogeneous, and brittle.

Subsequently, the specimens were again sealed into evacuated silica tubes, re-heated at 950°C (Cu,Zn,) and 530°C (Cu,Cd,) for 1-3 days and then cooled to room temperature.

Many such preparations had to be made of the Cu, Zn, phase to produce enough material, ~10 g, for neutron powder diffraction. A mixture of these several specimens was analyzed for copper electrolytically and for zinc by phosphate precipitation according to standard practice, and was found to have the desired composition to within 0.5 mole %.

The density measurements reported were carried out by weighing of the samples

in air and in chloroform.

Guinier photographs were taken, with  $CuK\alpha_1$  radiation ( $\lambda = 1.54050$  Å) and potassium chloride (a = 6.2919 Å) as an internal standard, of all individual alloy preparations. The  $\gamma$ -(Cu,Zn) specimens all had the same lattice parameter to within  $\pm 0.002$  Å. This was taken as evidence for their being identical in composition.

Single crystal X-ray intensity measurements were carried out, on a crystal of Cu, Cd, with a General Electric Diffractometer equipped with a full circle Single Crystal Orienter and a scintillation counter, using Ni-filtered  $CuK\alpha$  radiation and pulse height discrimination. Pulses were counted for 400 sec during a  $\theta$ -2 $\theta$  scan across each diffraction peak.

The crystal was a fairly irregular prism,  $\sim 50 \times 50 \times 100 \ \mu$ . 200 intensities were collected, with the crystal oriented so that absorption effects were likely to be minimized, corrected for absorption by approximate numerical integration and, applying the appropriate Lp-factors, converted to 80 independent structure factors.

For  $Cu_sAl_4$  the number of independent F's was 164. In the 10-cycle, full matrix refinements of  $Cu_5Cd_8$ , and also of  $Cu_5Al_4$ , the atomic scattering factors of Cromer and Waber  $^7$  and dispersion correction terms published by Cromer  $^8$  were employed, and Cruickshank's weighting function,  $w = (|F_0| \min + |F_0| + 2|F_0| \max^{-1} \cdot |F_0|^2)^{-1}$  was used.

Versions modified for the Uppsala CDC 3600 computer of World list  $^9$  programs No:s 6031 (Goniostat settings), 384 (Least-squares refinement) and an absorption program (not in the list), originally weighted by Coppens I respectively and Poblingwish, were used

(not in the list), originally written by Coppens, Leiserowitz and Rabinovich, were used.

The Cu<sub>5</sub>Zn<sub>8</sub> neutron powder diffraction record was prepared for us, as a chart recorder trace, by the Neutron Diffraction Group at the Swedish Research Councils' Laboratory, Studsvik. The sample holder was a cylindrical aluminum container,  $\emptyset = 10$  mm. The neutron wavelength was 1.07 Å. Experimental intensities were derived by graphical integration of the areas under the diffractometer chart peaks.

In the derivation of calculated intensities for various atomic distributions the neutron scattering factors and diffracted intensity expression listed by Bacon <sup>10</sup> were used. Thus,  $b_{\rm Zn} = 0.59 \times 10^{-12}$  cm and  $b_{\rm Cu} = 0.79 \times 10^{-12}$  cm. These calculations were performed on the computer TRASK, using a modified version of a program 11 written for the FACIT

computer (not in the World list).

#### GENERAL DESCRIPTION OF THE STRUCTURES

Cu<sub>5</sub>Zn<sub>8</sub> and Cu<sub>5</sub>Cd<sub>8</sub> have been reported to belong to space group No. 217, 143m<sup>2,3</sup> and Cu<sub>2</sub>Al<sub>4</sub> to space group No. 215, P43m.<sup>4</sup> No indications to the contrary have been found in the present investigation.

The structure type may be described in terms of two clusters, each comprising 26 atoms. One cluster, A, has its center at the origin 0,0,0; the other, B, is centered on  $\frac{1}{2},\frac{1}{2},\frac{1}{2}$ . In space group  $I\overline{4}3m$ , the clusters are identical, in space group  $P^{\overline{4}3m}$ , the atomic distributions in A and B are different, and the correspondence between position parameters in the two clusters is only approximate.

The clusters are built up of an Inner Tetrahedral position (IT), an Outer Tetrahedral position (OT), an Octahedral (OH), and a somewhat distorted Cubo-Octahedral (CO) position, with the following approximate parameters:

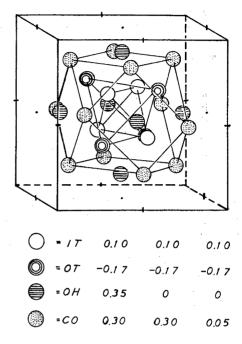


Fig. 1. Atomic sites in cluster A. IT = inner\_tetrahedral, OT = outer tetrahedral, OH = octahedral, and CO = cubo-octahedral position.

	$P\overline{4}3m$	$I\overline{4}3m$		Cluster A	Cluster B
IT OT OH CO	$egin{array}{c} 4(e) \ 4(e) \ 6(g) \ 12(i) \end{array}$	$8(c) \ 8(c) \ 12(e) \ 24(g)$	x,x,x; etc. x,x,x; * x,0,0; * x,x,z; *	$     \begin{array}{rcl}     x &=& 0.10 \\     x &=& -0.17 \\     x &=& 0.35 \\     x &=& 0.30 \\     z &=& 0.05     \end{array} $	$+(\frac{1}{2},\frac{1}{2},\frac{1}{2})$ in $I\overline{4}3m$ $+(\sim 0.50, \sim 0.50, \sim 0.50)$ in $P\overline{4}3m$ .

Fig. 1 shows the full complement of atomic sites in a cluster (A).

Final atomic distributions and refined parameters for the three structures are given in Table 5. Coordination and interatomic distances appear in Table 6.

## THE Cu, Zn STRUCTURE

The average value of the lattice parameter obtained in this investigation is:

$$a = 8.869 + 2 \text{ Å}$$

For the composition Cu<sub>5</sub>Zn<sub>8</sub>, with 52 atoms per unit cell, a comparison of measured and calculated densities yields:

$$d_{\rm obs} = 7.99 \text{ g cm}^{-3}, \qquad d_{\rm calc} = 8.01 \text{ g cm}^{-3}$$

The atomic positional parameters were fairly accurately determined by Bradley and Gregory<sup>3</sup> and are reproduced, with estimated standard deviations, in Table 5 alongside the refined parameters of the two other structures.

Table 1. Atomic dist	ribution mode	els for Cu	u,Zn,. Fo	r each mo	del, the s	ymbol Cu,Zn signifies
a random	distribution	of Cu	and Zn	over all	sites so	designated.

Model	IT	ОТ	ОН	со	Туре
A B C D E F	Zn Cu,Zn Zn Cu Cu Cu,Zn	Cu Cu,Zn Cu Cu Cu Cu,Zn	Cu Cu,Zn Cu,Zn Cu,Zn Cu,Zn	Zn Zn Cu,Zn Cu,Zn Cu,Zn Cu,Zn	Au <sub>s</sub> Zn <sub>s</sub> Cu <sub>s</sub> Cd <sub>s</sub> Random

Table 1 summarizes the atomic distribution models tested and Table 2 gives their fit with the observed neutron diffraction intensities. The completely ordered Au<sub>5</sub>Zn<sub>8</sub> type distribution, model A, is seen to give the best agreement with the observations. The somewhat randomized versions, B and C, of the distribution type might conceivably be considered to give an acceptable fit, so that a certain measure of substitution of Cu for Zn and vice versa, can not be completely ruled out. The Cu<sub>5</sub>Cd<sub>8</sub> type distribution model, E, a slightly more ordered version thereof, D, and the completely random distribution, model F, are definitely poorer and can be eliminated.

Table 2. Observed and calculated neutron diffraction intensities for Cu<sub>5</sub>Zn<sub>8</sub>. Distribution models as in Table 1.

$h \ k \ l$	$I_{ m obs}$			7	calc		
	2005	A	В	C	D	E	F
211	11	15	8	8	7	4	2
220	_	0	0	0	0	0	0
310		0	0	0	0	1	0
222	10	9	14	13	14	17	16
321	12	9	13	12	12	14	14
400	_	0	0	0	0	1	0
420	_	<b>2</b>	3	3	3	3	3
332	18	17	22	19	26	26	19
422	20	19	18	15	19	19	11
510, 431	8	7	11	10	9	16	12
521		1	2	4	2	3	5
440	_	1	2 2 2	${ 2 \atop 4 }$	3	4	2 2
433, 530		2	2	4	1	2	2
600, 442	<b>54</b>	62	57	60	<b>52</b>	49	44
611, 532	14	11	11	9	11	9	8
620		0	0	0	0	0	0
541		3	<b>2</b>	2 1	2	4	1
622	_	0	$_{1}^{2}$	1	1	1	1
631; 444; 710, 550, 543; 640	80	76	87	79	83	86	73
633, 721, 552	147	148	147	144	138	133	116
642		5	6	6	6	6	6
730	_	3	3	$\ddot{2}$	$\tilde{2}$	$\dot{2}$	2
732, 651	11	11	15	$1\overline{3}$	15	$1\overline{7}$	13

Table 3. Structure factors for final refined model of  $Cu_sCd_s$ . R = 11 %.

011         0         6           002         47         30           112         28         42           022         48         47           222         311         362           013         194         185           123         233         202           033         776         891           233         313         363           004         145         170           114         663         671           024         46         48           224         344         301           134         94         82           334         121         114           044         85         93           244         237         218           444         574         633           015         161         174           125         80         61           035         156         125           235         154         122           145         190         177           345         112         99           055         625         473	266 466 666 017 127 037 237 147 347 057 257 457 167 367 077 277 008 118 028 228 138	261 94 287 81 359 83 170 237 99 46 229 137 71 58 96 86 216 32 204 182	252 81 274 84 386 93 172 222 81 36 230 126 66 77 75 238 21 214
002       47       30         112       28       42         022       48       47         222       311       362         013       194       185         123       233       202         033       776       891         233       313       363         004       145       170         114       663       671         024       46       48         224       344       301         134       94       82         334       121       114         044       85       93         244       237       218         444       574       633         015       161       174         125       80       61         035       156       125         235       154       122         145       190       177         345       112       99         055       625       473         255       141       113         455       106       116         006       291       270 <td>466 666 017 127 037 237 147 347 057 257 457 167 367 077 277 008 118 028 228</td> <td>94 287 81 359 83 170 237 99 46 229 137 71 58 96 86 216 32 204 182</td> <td>81 274 84 386 93 172 222 81 36 230 126 66 77 75 238 21</td>	466 666 017 127 037 237 147 347 057 257 457 167 367 077 277 008 118 028 228	94 287 81 359 83 170 237 99 46 229 137 71 58 96 86 216 32 204 182	81 274 84 386 93 172 222 81 36 230 126 66 77 75 238 21
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004     145     170       114     663     671       024     46     48       224     344     301       134     94     82       334     121     114       044     85     93       244     237     218       444     574     633       015     161     174       125     80     61       035     156     125       235     154     122       145     190     177       345     112     99       055     625     473       255     141     113       455     106     116       006     291     270       116     113     123       026     133     140       226     190     200       136     298     255	257 457 167 367 077 277 008 118 028 228	229 137 71 58 96 86 216 32 204 182	36 230 126 66 66 77 75 238 21
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334     121     114       044     85     93       244     237     218       444     574     633       015     161     174       125     80     61       035     156     125       235     154     122       145     190     177       345     112     99       055     625     473       255     141     113       455     106     116       006     291     270       116     113     123       026     133     140       226     190     200       136     298     255	077 277 008 118 028 228	$\begin{array}{c} 96 \\ 86 \\ 216 \\ 32 \\ 204 \\ 182 \end{array}$	77 75 238 21 214
044     85     93       244     237     218       444     574     633       015     161     174       125     80     61       035     156     125       235     154     122       145     190     177       345     112     99       055     625     473       255     141     113       455     106     116       006     291     270       116     113     123       026     133     140       226     190     200       136     298     255	277 008 118 028 228	$egin{array}{c} 86 \\ 216 \\ 32 \\ 204 \\ 182 \\ \end{array}$	75 238 21 214
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125     80     61       035     156     125       235     154     122       145     190     177       345     112     99       055     625     473       255     141     113       455     106     116       006     291     270       116     113     123       026     133     140       226     190     200       136     298     255	228	182	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	228	182	
235     154     122       145     190     177       345     112     99       055     625     473       255     141     113       455     106     116       006     291     270       116     113     123       026     133     140       226     190     200       136     298     255	190		202
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		32	30
345     112     99       055     625     473       255     141     113       455     106     116       006     291     270       116     113     123       026     133     140       226     190     200       136     298     255	<b>33</b> 8	151	165
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	048	59	50
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	<b>248</b>	34	34
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	448	129	137
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	158	115	130
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	<b>35</b> 8	208	228
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	068	102	96
226 190 200 136 298 255	<b>268</b>	40	38
136 298 255	019	60	62
	129	92	96
	039	41	42
336 352 349	696	95	109
046 79 73	239	149	166
246 159 136	149	142	
446 188 188	$\begin{array}{c} 149 \\ 349 \end{array}$	47	63
156 203 164	149 349 059	$\begin{array}{c} 47 \\ 202 \end{array}$	63 187
356 160 137	149 349 059 00.10	$\begin{array}{c} 47 \\ 202 \\ 170 \end{array}$	63 187 193
556 80 67 066 397 301	149 349 059	$\begin{array}{c} 47 \\ 202 \end{array}$	63 187 193 158

A few other models, with inverted distributions of Cu and Zn have also been tried. The calculated neutron diffraction intensities for all these models were completely at variance with the observed data.

## THE CusCds STRUCTURE

The lattice parameter of the investigated sample is:

$$a = 9.5888 \pm 3$$
 Å.

Table 4. Structure factors for refined model of  $Cu_9Al_4$ . R=14.5 %.

						y <b>4</b>	1110 /01	
hkl	$ F_{ m o} $	$ F_{\rm c} $	hkl	$ F_{\rm o} $	$ F_{\rm c} $	hkl	$ F_{\mathrm{o}} $	$ F_{c} $
001 011 111	38	33	006	321	401	077	25	22
011	29 33	<b>22</b>	016 116 026 126	43	42	177	31	$\frac{22}{32}$
111	33	21	116	43 99	42 93	277	123	99
002	31	$2\overline{4}$	026	18	7	377	28	30
002 012	71	54	126	25	19	477	$2\overline{45}$	242
112	71 105 10	80	996	33	26	008	47	46
099	100	9	226 036 136 236	50	44	018	14	16
022 122 222	04	67	190	114	100	118	41	
000	84 147		100	114	108 32	110	100	38
222	147	124	230	59 114 33 318	32 99 <i>c</i>	028	106	109
003 013	163	151	336	318	336	128 228	21	23
013	21	19	046	91	87	228	94	94
113	37	26	146	40	37	038 138	47	53
023	13	14	246	$\begin{array}{c} 65 \\ 32 \end{array}$	61	138	49	54
123	<b>74</b>	55	346	32	27	238	32	36
223	50	38	446	96	89	238 338	60	58
023 123 223 033 133 233 333	427	672	056	47	<b>52</b>	048	38	30
133	49	39	156	47	49	148	31	36
233	149	129	256	37	31	248	24	28
333	122	129 93	356	71	<b>54</b>	348	11	15
004	11	6	456	16	13	448	20	20
014	10	8	556	34 276 20	30	058	18	25
114	276	345	066	276	292	158	29	28
024	67	51	166	20	22	258	$\frac{20}{27}$	33
194	50	40	266	134	124	358	151	148
024 124 224	164	144	366	42	29	458	25	24
430	97	22	466	47	41	558	93	90
134	27 43	37	566	12	16	068	<b>49</b>	48
234	51	43	666	205	155	168	20	21
334	57		000	44	49	268	20 20	70
044	57 58	47	007	11		200	68 28 28 8 52	30
144	98	48	017		4	368	28	
144	69	56	117	$5\underline{4}$	52	468	28	29
244	213	184	027	7	6	078	8	2
344	19	17	127	203	215	178	52	67
444	<b>33</b> 0	372	227 037	30 70	27	278	34 23	43
005	14	13	037	70	70	009	23	4
015	84	72	137	24	21	019	63	72
115	72	65	237	83	84 37	119	63 32	33
005 015 115 025	11	<b>2</b>	337	83 35 23	37	029	$\begin{array}{c} 10 \\ 42 \end{array}$	3
125 225 035 135	28	21	047	23	18	129	42	<b>5</b> 0
<b>225</b>	64	59	147	222	232	229 039	40	. 40
035	13	9	247	12	7	039	166	162 16
135	44	35	347	51	47	139 239	14	16
235	68	59	447	69	75	239	40	36
335	37	35	057	12	9	339	25	25
045	55	51	157	12 12	13	049	28	31
145	59	41	257	98	91	149	81	92
245	25	23	357	98 11 112	5	249	28 81 9	8
345	70	23 56	457	110	5 98	349	47	46
445	94	90 90	407	114	90 94	440		
445 055	34 203 32 123	28	557	25	24	449	19	21
000	203	208 29	067	16	14	059	$\begin{array}{c} 32 \\ 17 \end{array}$	35
155	32	29	167	31	30 18	059 159 259	17	15
255	123	109	267	19	18	259	35	46
355	17	18	367	37	30	359	6	10
455	<b>7</b> 5	68	467	16	20	069	25	23
555	62	63	567	42	38			

The positional parameters of Ref. 3 were used as a starting point for refinements of four different distribution models, viz.

A) a Cu<sub>5</sub>Zn<sub>8</sub> (Au<sub>5</sub>Zn<sub>8</sub>) type distribution

B) model A with Cu and Cd interchanged between IT and OT

C) the Cu<sub>5</sub>Cd<sub>8</sub> type reported in Ref. 3.

D) a completely random distribution of Cu and Cd over all sites.

The residual,  $R=\sum ||F_{\rm o}|-|F_{\rm c}||/\sum |F_{\rm o}|$ , at the end of each refinement was  $R_{\rm A}=0.25,~R_{\rm B}=0.24,~R_{\rm C}=0.11~$  and  $R_{\rm D}=0.16$ 

Thus, of the models tested, C is obviously the best one. This is also substantiated by the fact that the refinement of C yielded the lowest standard deviations in all parameters. The result is listed in Table 5. A comparison of observed and calculated structure factors is given in Table 3.

It was not considered necessary to test any further models, since the final individual thermal parameters in each of the cases A, B, and D showed what was amiss with the model. An excess of Cd with respect to model C, at any site, showed up as a very high B value and an excess of Cu, naturally, as a very low (negative) B.

The average temperature factor value for model C is  $\overline{B} = 1.6 \text{ Å}^2$ , which is within two standard deviations of all individual B's.

The weight analyses, both according to  $|F_o|$  and according to  $\sin^2\theta$ , were without significant trend and remarkable excursions, except as regards the three of four strongest reflections.

Table 5. Atomic distributions, positional and thermal parameters in the refined structures. Cu<sub>8</sub>Zn<sub>8</sub> parameters from Bradley and Gregory.<sup>3</sup> The symbol, Cd,Cu signifies a random occupation of the site by Cd and Cu in the ratio 8:1.

		$\mathrm{Cu_5Zn_8}$	$\mathrm{Cu_5Cd_8}$	Cu <sub>g</sub> .	Al <sub>4</sub> Cluster B
				Clustel A	
	$a\pm\sigma ext{\AA}$	$8.869\pm2$	$9.5888\pm3$	8.702	$3\pm 5$
IT	$egin{array}{l}  ext{Atom} \ x  \pm  \sigma \ B  \pm  \sigma   ext{Å}^2 \end{array}$	$\overset{\mathbf{Zn}}{\overset{0.110}{1}} \pm 3$	$0.0939 \pm 11$	$\begin{array}{c} & \text{Al} \\ 0.1144 \pm 17 \\ -0.1 \pm 3 \end{array}$	$0.6046\pm7$
ОТ	$egin{array}{l} { m Atom} \ x  \pm  \sigma \ B  \pm  \sigma  { m \AA}^2 \end{array}$	$\substack{-0.172 \pm 3 \\ 1}$	$^{\mathrm{Cu}}_{-0.1617\pm12}_{1.2\pm4}$	$^{\mathrm{Cu}}_{-0.1690\pm9}\\_{0.3\pm3}$	$egin{array}{c} { m Cu} \\ { m 0.3248}  \pm  9 \\ { m 0.3}  \pm  2 \end{array}$
ОН	$egin{array}{l} { m Atom} \ x  \pm  \sigma \ B  \pm  \sigma  { m \AA}^2 \end{array}$	$^{\mathrm{Cu}}_{0.355~\pm~3}$	$^{\rm Cd,Cu}_{0.3506~\pm~9}_{2.0~\pm~2}$	$egin{array}{c}  ext{Cu} \\ 0.3565 \pm 10 \\ 0.0 \pm 2 \end{array}$	$egin{array}{c} { m Cu} \\ { m 0.8554}  \pm  10 \\ { m 0.0}  \pm  2 \end{array}$
CO	$egin{array}{l}  ext{Atom} \ x  \pm  \sigma \ z  \pm  \sigma \ B  \pm  \sigma   ext{\AA}^2 \end{array}$	$egin{array}{c}  ext{Zn} \\ 0.313 \pm 3 \\ 0.036 \pm 3 \\ 1 \end{array}$			$\begin{array}{c} \text{Al} \\ 0.81081 \pm 12 \\ 0.53671 \pm 16 \\ 0.4 \pm 3 \end{array}$

Table 6. Coordination, number and type of contacts, and interatomic distances (Å), with standard deviations, in the  $\gamma$ -phases.

		$\mathrm{Cu_5Zn_8}$	$\mathrm{Cu_5Cd_8}$	$\mathrm{Cu}_{\mathfrak{g}}\mathrm{Al}_{4}(\mathbf{A})$	$\mathrm{Cu}_{9}\mathrm{Al}_{4}(\mathrm{B})$
3 IT	$\Gamma(A) - IT(A)$	Zn—Zn 2.75	$rac{ ext{Cu}- ext{Cu}}{2.574\pm24}$	$\begin{array}{c} \text{Al-Al} \\ 2.815 \pm 33 \end{array}$	$\begin{array}{c} { m Cu-Cu} \\ 2.574\pm14 \end{array}$
3	$-\mathrm{OT}(\mathbf{A})$	—Cu 2.61	$^{-\mathrm{Cu}}_{2.618~\pm~17}$	$^{-\mathrm{Cu}}_{2.556~\pm~14}$	$^{- ext{Cu}}_{2.585~\pm~11}$
3	-OH(A)	—Cu 2.57	$^{\rm -Cd}_{\rm 2.771~\pm~8}$	$-\mathrm{Cu} \ [2.534 \pm 7]$	$^{-\mathrm{Cu}}_{2.534~\pm~8}$
3	—CO(A)	— <b>Z</b> n 2.62	$^{\rm -Cd}_{2.789~\pm~15}$	$-\mathrm{Cu} \\ 2.557 \pm 18$	$\begin{array}{c} -\text{Al} \\ 2.605 \pm 11 \end{array}$
3 O	$\Gamma(A) - IT(A)$	$\begin{array}{c} \mathrm{Cu-Zn} \\ 2.61 \end{array}$	${^{ m Cu-Cu}}_{2.618~\pm~17}$	$egin{array}{l} \mathrm{Cu\!-\!Al} \ 2.556\pm14 \end{array}$	$^{\mathrm{Cu-Cu}}_{2.585~\pm~11}$
3	—OH(A)	—Cu 2.69	$^{-\mathrm{Cd}}_{2.844~\pm~8}$	$^{-\mathrm{Cu}}_{2.643~\pm~7}$	$^{\rm -Cu}_{\rm 2.666~\pm 7}$
3	$-\mathrm{CO}(\mathrm{A})$	—Zn 2.55	$^{-\mathrm{Cd}}_{2.800~\pm~7}$	$^{-\mathrm{Cu}}_{2.511~\pm~7}$	$\begin{array}{c} -\text{Al} \\ 2.487 \pm 14 \end{array}$
3	-CO(B)	—Zn 2.59	$\begin{array}{c} -\mathrm{Cd} \\ 2.746 \pm 16 \end{array}$	$-\mathrm{Al} \\ 2.573 \pm 17$	$-\mathrm{Cu} \\ 2.536 \pm 10$
2 01	H(A) - IT(A)	$\begin{array}{c} \mathrm{Cu}\!-\!\mathrm{Zn} \\ 2.57 \end{array}$	$\begin{array}{c} { m Cd-Cu} \\ 2.771 \pm 8 \end{array}$	$\mathrm{Cu}\mathbf{-Al} \ 2.534\pm7$	$\begin{array}{c} { m Cu-Cu} \\ { m 2.534} \pm 8 \end{array}$
2	-OT(A)	—Cu 2.69	$-\mathrm{Cu} \\ 2.844 \pm 8$	$-\mathrm{Cu} \\ 2.643 \pm 7$	$^{-\mathrm{Cu}}_{2.666~\pm~7}$
1	-OH(A)	—Cu 2.56	$\begin{array}{c} -\mathrm{Cd} \\ 2.865 \pm 17 \end{array}$	$-\mathrm{Cu} \\ 2.497 \pm 17$	$-\mathrm{Cu} \\ 2.517 \pm 17$
4	-CO(A)	Zn 2.81	$\begin{array}{c} -\mathrm{Cd} \\ 2.954 \pm 4 \end{array}$	$\begin{array}{c} -\mathrm{Cu} \\ 2.774 \pm 5 \end{array}$	$\begin{array}{c} -\mathbf{Al} \\ 2.751 \pm 9 \end{array}$
2	CO(B)	—Zn 2.53	$\begin{array}{c} -\mathrm{Cd} \\ 2.877 \pm 7 \end{array}$	$-\mathrm{Al} \atop 2.507\pm15$	$\begin{array}{c} -\text{Cu} \\ \textbf{2.482} \pm 8 \end{array}$
2	-CO(B)'	-Zn 2.83	$\begin{array}{c} -\mathrm{Cd} \\ 3.383 \pm 8 \end{array}$	$-\text{Al} \\ 2.808 \pm 15$	$\begin{array}{c} -\mathrm{Cu} \\ 2.764 \pm 9 \end{array}$
1 CC	O(A) —IT(A)	$     \begin{array}{c}       \operatorname{Zn} - \operatorname{Zn} \\       2.62    \end{array} $	$\begin{array}{c} { m Cd-Cu} \\ { m 2.789~\pm~15} \end{array}$	$\begin{array}{c}  ext{Cu-Al} \\  ext{2.557} \pm 18 \end{array}$	$\begin{array}{c} \text{Al-Cu} \\ 2.605 \pm 16 \end{array}$
1	-OT(A)	—Cu 2.55	$-\mathrm{Cu}_{2.800~\pm~7}$	$\begin{array}{c} -\mathrm{Cu} \\ 2.511 \pm 7 \end{array}$	$-\mathrm{Cu} \\ 2.487 \pm 14$
2	—OH(A)	Cu 2.81	$\begin{array}{c} -\mathrm{Cd} \\ 2.954 \pm 4 \end{array}$	$\begin{array}{c} -\mathrm{Cu} \\ -\mathrm{Cl} \\ 2.774 \pm 5 \end{array}$	$\begin{array}{c} -\mathrm{Cu} \\ 2.751 \pm 9 \end{array}$
1	-OT(B)	—Cu 2.59	$-\mathrm{Cu} \\ 2.746 \pm 16$	$-\mathrm{Cu} \\ 2.536 \pm 10$	$-\mathrm{Cu} \\ 2.573 \pm 17$
1	-OH(B)	Cu 2.53	$-\mathrm{Cd} \atop 2.877 \pm 7$	$-\mathrm{Cu} \\ 2.482 \pm 8$	$-Cu$ $2.507 \pm 15$
1	-OH(B)'	-Cu 2.83	$\begin{array}{c} -\mathrm{Cd} \\ 3.383 \pm 8 \end{array}$	$-\mathrm{Cu} \\ 2.764 \pm 9$	$-Cu$ $2.808 \pm 15$
4	-CO(B)	-Zn 2.63	$-\mathrm{Cd} \atop 2.994 \pm 4$	$-{\rm Al}\atop 2.575\pm 9$	$-\mathrm{Cu} \\ 2.575\pm9$
2	—CO(B)'	-Zn 2.63	$-\mathrm{Cd} \\ 3.259 \pm 12$	$-\text{Al} \\ 2.601 \pm 11$	$-\text{Cu} \\ 2.601 \pm 11$
		2.00	3.200 12	J.002 11	<b></b>

The differences between the refined position parameters and those of Bradley and Gregory 3 are of the order of 0.002 units. It is to be expected that the accuracy of their Cu<sub>5</sub>Zn<sub>8</sub> parameters is as good, or better.

## THE Cu.Al. STRUCTURE

The observed lattice parameter:

$$a = 8.7023 \pm 5 \text{ Å}.$$

and atomic positional and thermal parameters taken from Ref. 5 were used as a starting point for the computations. The shifts obtained in the atomic positions were within the standard deviations of the present refinement (which are a little larger than those of Ref. 5) except for the shift in the CO(B) parameter  $x_{Al}$ , which was approximately 1.5 standard deviations.

The significant changes occurred in the individual thermal parameter values which now lie mostly within one standard deviation (2 s.d.'s for Cu<sub>IT(B)</sub>) from their average value,  $\overline{B} = 0.1 \text{ Å}^2$ . This is taken as evidence that the atomic distribution is the correct one. (That the value of  $\overline{B}$  is so small may indicate an insufficiently large correction for absorption). The standard deviations of the B's had obviously also been quite erroneously calculated by the program available in the previous investigation.<sup>5</sup> The present ones are about five times larger.

Structure factors are listed in Table 4, refined parameters and interatomic distances in Tables 5 and 6, respectively.

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